

1. Summary

AWA 8 Watt Amplifier Type PA774, S.N. AF 9919. HRSA Feb 2023

1.1 Original design

One microphone and one P.U. input channel PA amplifier. Half 12AX7 amplifier for MIC channel. PU input summing into half 12AX7 summing amplifier. 6BM8 floating paraphrase splitter provides high gain to PP pentode output stage. Cathode bias push-pull 6BM8 output, with isolated secondary feedback winding taken to the 2nd stage cathode. 220V plate supply from FC442 bridge diode rectifier and capacitor filter. Plate supply fed direct to the screen supply. Cascading resistor/cap dropping to the splitter voltage supply, and again to the input amp supplies. 6.3VAC heater supplied to all valves, and hum cancelling feedback taken to cathode of V3B. Vol pot for MIC input. Vol pot for P.U. input. Tone pot for P.U. input. Output load settings 150/300/600/1200 Ω from 5K PP transformer.

Appears complete with only minor mods. Transformers marked with '60720' and BD?; and '60195' and BC?. Ducon caps with 2671, 2271 datecodes. Mustard with A4H. UCC caps with 2064 and 2264 datecode. Modifications noted were: caps and IRC WW's with 70 19 datecodes. 6BM8 datecodes VM15 (1970 Dec) and WG20 (1971, Jul); Problems included: bad ecap cans; hard and cracking wire insulation; R14 1k65; R17-R19 >10%.

1.2 Modified Design for Guitar Amp use

- Replaced AC mains cable with side-wall mounted IEC/fuse/switch/indicator combo. 0.8A IEC T 5x20.
- Primary wiring direct to -10 and 240V PT terminals, with S14K300 MOV.
- 1k screen stoppers.
- HT UF4007 bridge rectifier to 47 μ F 400V, to 100R 2W to 47 μ F 400V.
- 270 Ω 3W common cathode with 100 μ F 50V, then 10 Ω to each cathode.
- Shorting guitar 6.5mm isolated input socket with 1M Ω load and 10k grid stopper.
- 150k Ω anode loads for both preamp stages, with un-bypassed 2k2 cathodes. 12AU7 used.
- C1 lowered from 22nF to 4nF. C3 lowered from 47nF to 10nF. C4&C6 lowered from 22nF to 10nF.
- Relocate tone and vol pot to before PI stage. Tone pot across vol pot for treble drop. Phono Vol pot across R26, with 1.2nF from wiper to 0V for treble gain.
- Balanced PI gains for reduced distortion.
- 2502 GEAQ MOVs on OPT pri.
- Fixed OPT output from 150 to 300 taps for 25 Ω load, to shorting 6.5mm socket for 16 Ω speaker. Removed wiring from COM and 1200. Grounded 150 tap.
- Added 5-pin maintenance socket for bias and VS1/100 monitoring.

Inputs reduced to just one guitar input – isolated 6.5mm socket with tip grounded; changed R1 to 1M and 10K grid input added; R2 and R9 changed to 2K2; R4 & R11 changed to 150K. PU circuitry and summer removed.

2. Measurements

Mains circuit IR >2G at 1kVdc.

PP circuit IR >2G at 1kVdc.

Voltage rail regulation.

Rail	Idle	5.2Wpk output
VS raw	234V (2.67Vrms)	
VS1	228V (0.85Vrms)	213V
VS2	222V (30mVrms)	208V
VS3	218V	
Heater 1	6.25	
Cathodes	16.5V, 32/32mA (6.8W, 6.8W)	47/47mA

Power transformer primary DC resistance: 62Ω. BL, GRY, OR, Y, (-10, 0, 220, 240)

Power transformer secondary DC resistance: 71Ω.

12VAC 50Hz nominal applied to output transformer 150R winding

Winding	Volts rms	Turns ratio; Pri Impedance; Spec level; Notes; turns %
Pri P-P: BLU to Vi	70.92	1 ; ; N/A; appears to be 5k P-P
Sec: Feedback; 16Ω dcr	7.04	10.07; N/A; 49Ω, based on 5k P-P 20.2
Sec: 150 to Com; 5Ω dcr	12.33	5.75; 4,960Ω; 150 Ω; based on 150 35.5
Sec: 300 to Com	17.43	4.07; 4,970Ω; 302Ω; based on 5k P-P 50.1
Sec: 1200 to Com; 18Ω dcr	34.79	2.04; 4,994Ω; 1201Ω; based on 5k P-P 100
Sec: 150 to 300; 2.2Ω dcr	5.04	14.07; N/A; 25.2Ω; based on 5k P-P 14.5
Sec: 1200 to 300; 9Ω dcr	17.28	4.1; N/A; 300Ω; based on 5k P-P 50

1200Ω winding stated as 100Vac, indicating 204Vac PP primary rated, and 20.4Vac feedback.

300 = OR; 150 = GR; 1200 = GRY; COM= Y

Feedback winding is sandwiched between inner prim, and outer secondary (1200 as outermost tap).

150 and 300 taps come out as a pair, so could be split.

Output transformer primary DC resistance: 77+73= 150Ω plate-to-plate.

DCR dissipation in OPT primary at idle is $150 \times 0.033^2 = 0.16W$, which could increase to circa 0.4W if cranked. If the COM-150 and the 150-1200 winding sections were joined, the resulting DCR=14 could likely support at least 300mAdc (constant 1.3 to 1.5W) as they are the outermost windings. The peak nI of a half primary is circa $102V_t \times 0.1A = 10$ for a peak 100mA. An equivalent nI for the special secondary would be $85V_t \times 0.12A$. The dc volt drop at 0.12A is ~2V.

6BM8 matched pair 44,54 show 44 conducts first and takes full conduction for a few seconds.

Swapped 44,55 pair in V2 & V3 locations to get balanced pentode drive levels. AC balance pot can null out 2HD, with 3HD remaining fairly constant.

Output to 9Vrms (5.2W) peak into 15.5Ω load. Distortion is quite low, rising above 4Vrms (1W), with 9Vrms (pk output setting) sinewave showing some cross-over distortion and one side starting to soft-clip, with gross overload causing severe clipping and Vrms reducing.

Feedback level 3.8dB with R8 disconnected.

- 1W distortion 0.5% THD from 300Hz to 1kHz, and rising outside, with nearly equal 2nd and 3rd, but 2nd dominant at higher frequencies.
- 4W distortion 5% THD from 50Hz to 3kHz, with 3rd dominant and flat, until 2nd dominates above 5kHz.

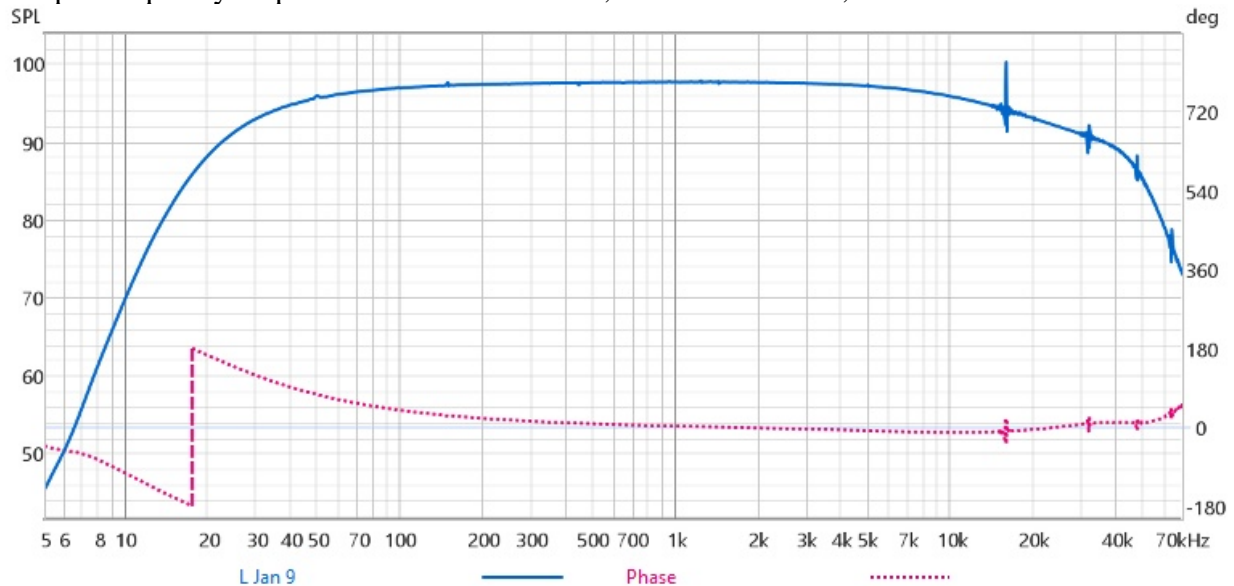
Signal gain for 6Vrms output on 15.5Ω, with tones at min and Vol at max.

- RV3 top at 15mV (RV3 at max)
- Input ~0.76mV, so first stage gain abt 20x.
- from V2A triode input to V2B pentode input ~ $9V/0.18V = 50x$.

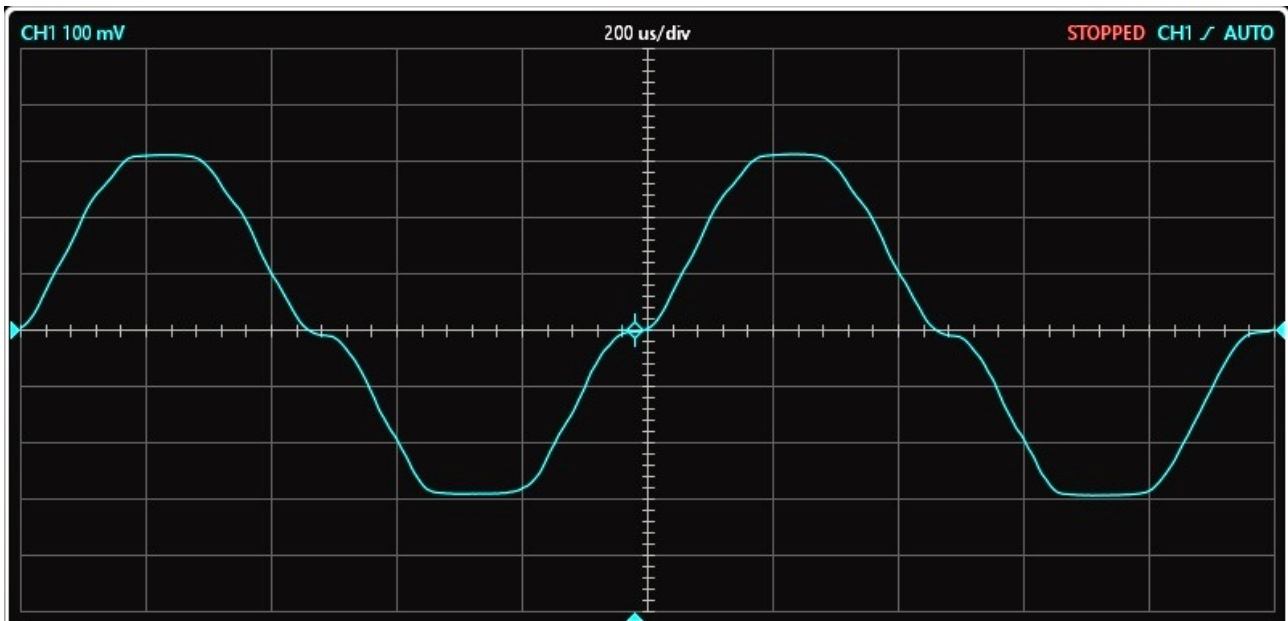
240Vac mains has heater voltage sitting at 6.25Vac at idle.

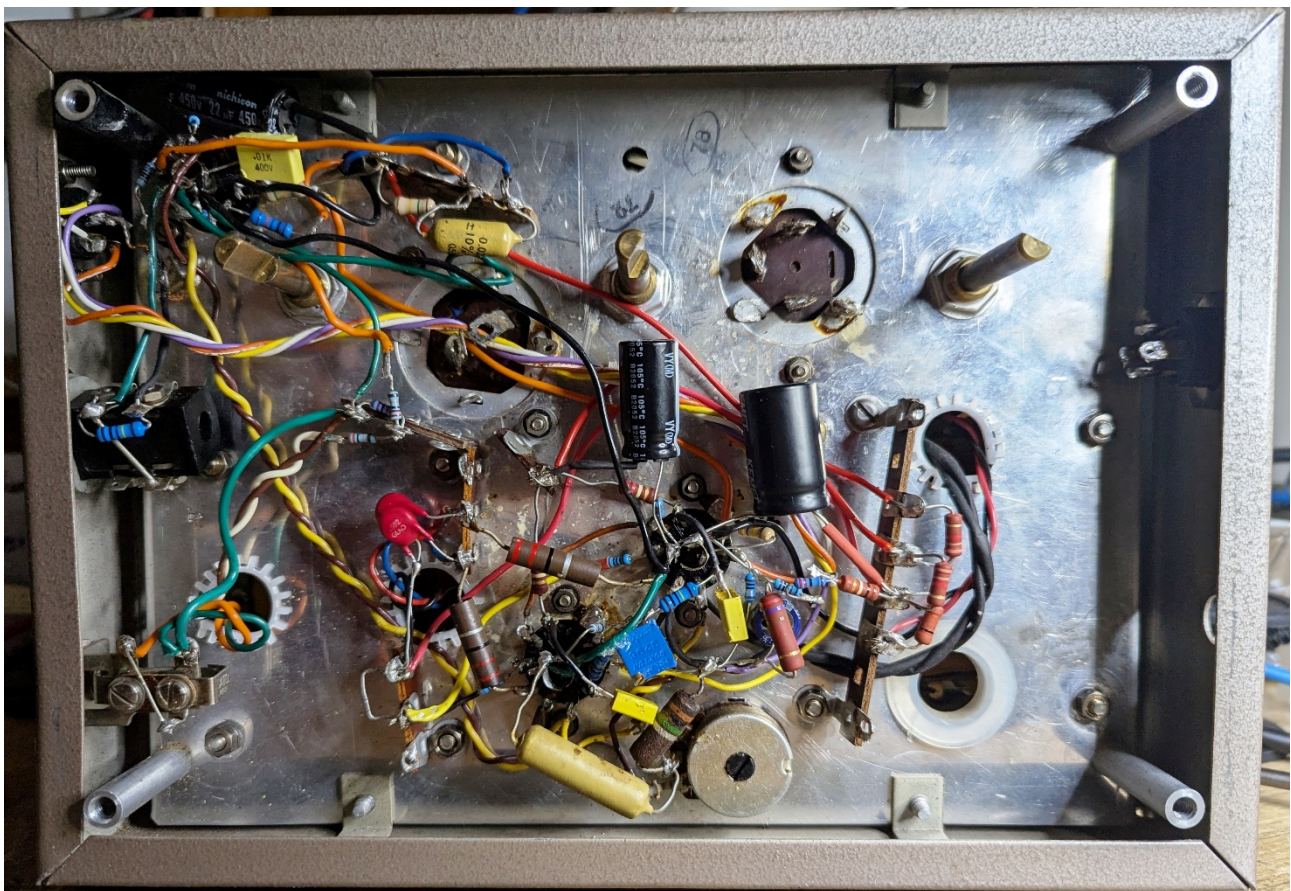
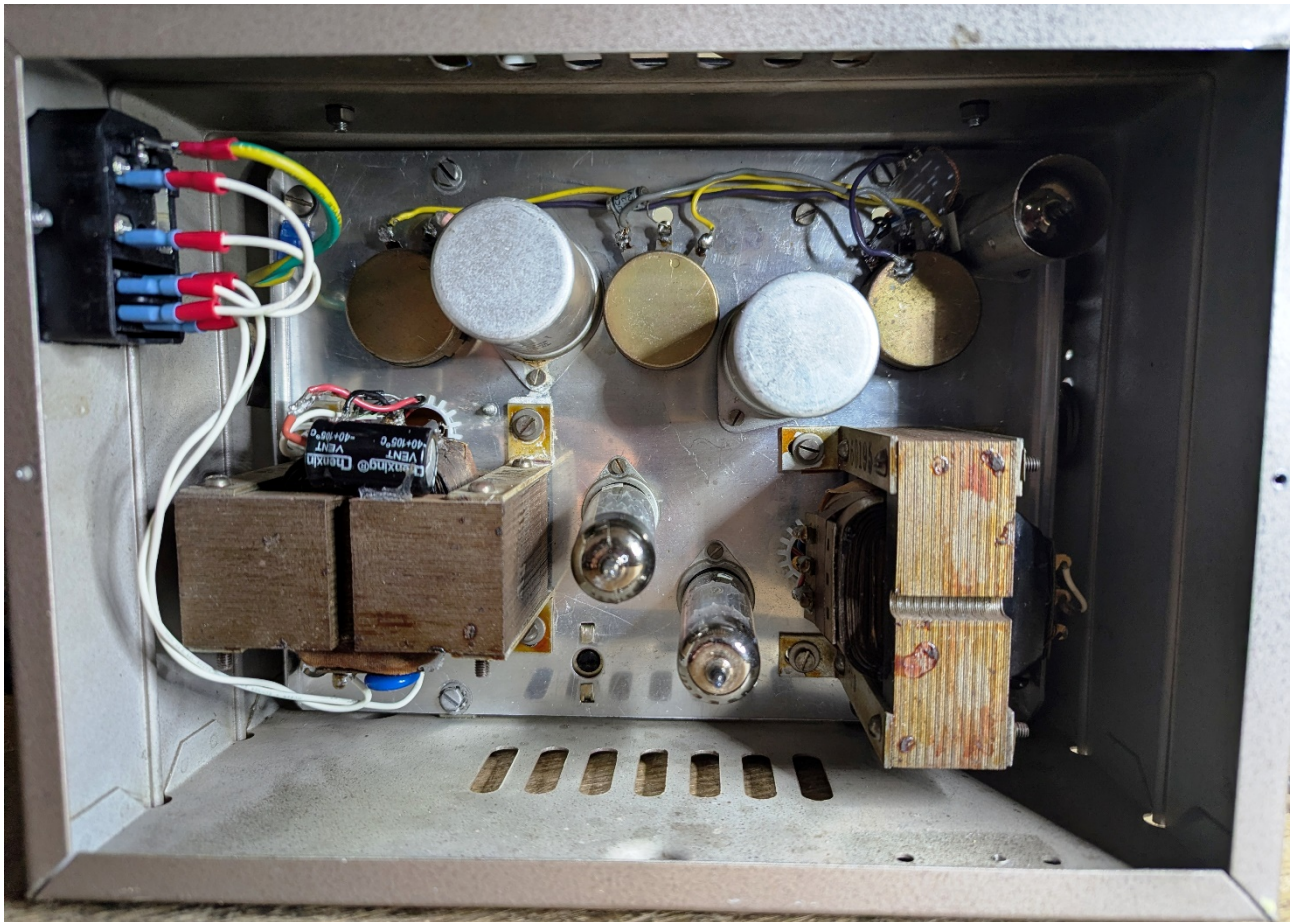
Phono Vol gives +5dB at 2-3kHz at max, and flat at min, but depends on Mic Vol setting.
Phono tone gives treble cut from -2dB at 10kHz at max, to 2-3kHz corner and -9dB at 10kHz at min.

Example frequency response for Mic Vol = 90%, Phono Vol = min; Phono Tone = max.



5.4W cranked 1kHz waveform.

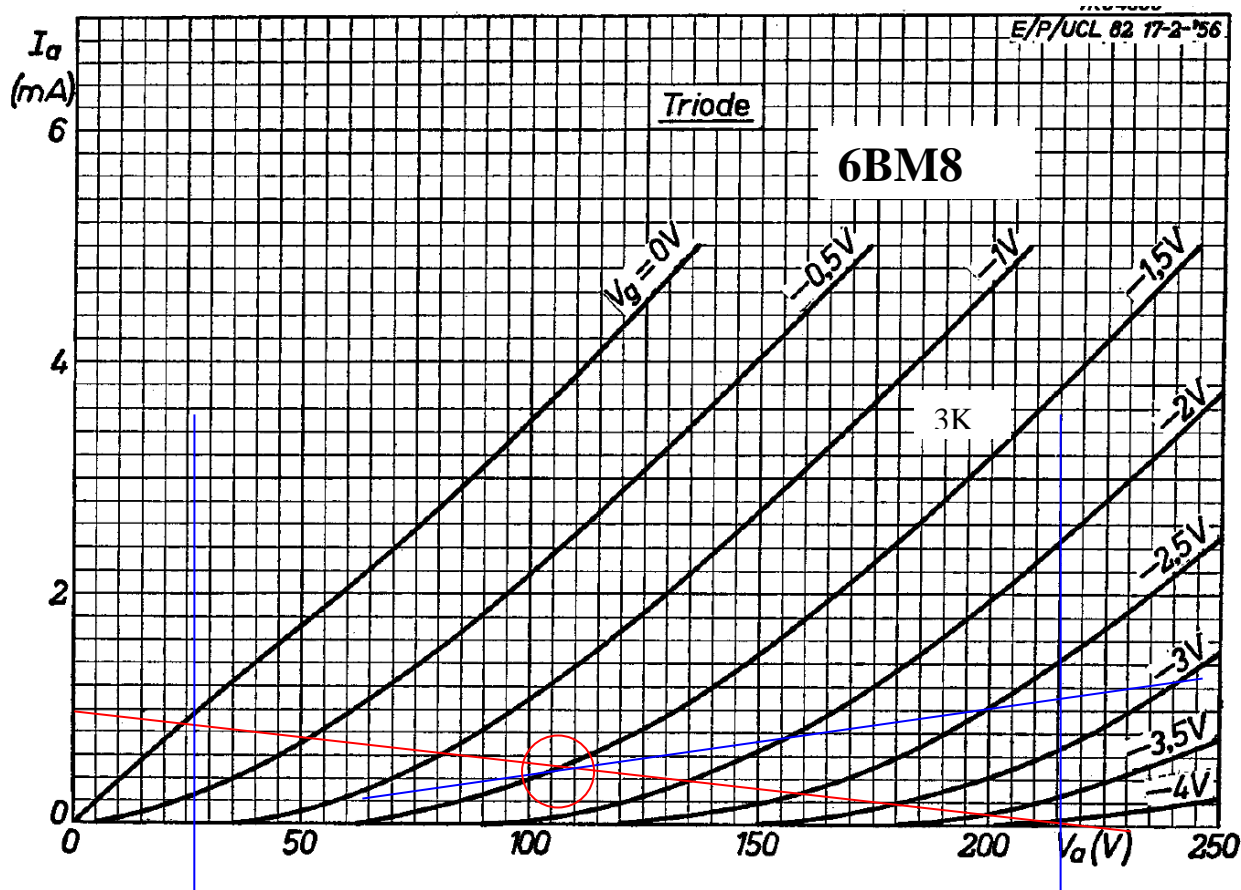




3. Design Info

3.1 Splitter stage – 6BM8 Triode

Cathode-coupled floating paraphase configuration phase splitter [Carpenter, Scroggie WW 1945] but with additional simplified/economy of parts. The output stage grid leaks form part of the floating difference signal presented to V3A, and the common cathode arrangement of the PI does not require capacitor bypass. An added 100k trimpot allows nulling of second harmonic level of the output, and sits at nominal ground voltage.



3.2 Output Stage

In this Class AB push-pull output stage, one tube is pushed into conduction and the other tube is pulled into cutoff, and there is a region of overlap where both tubes conduct equivalent levels of current. The cathodes are biased to +18V using a common cathode resistor. The 5K Ω impedance plate-to-plate OPT presents each tube with a 1.25K Ω load impedance (with a matched secondary load) for signal currents in Class B region, and 2.5K in Class A region.

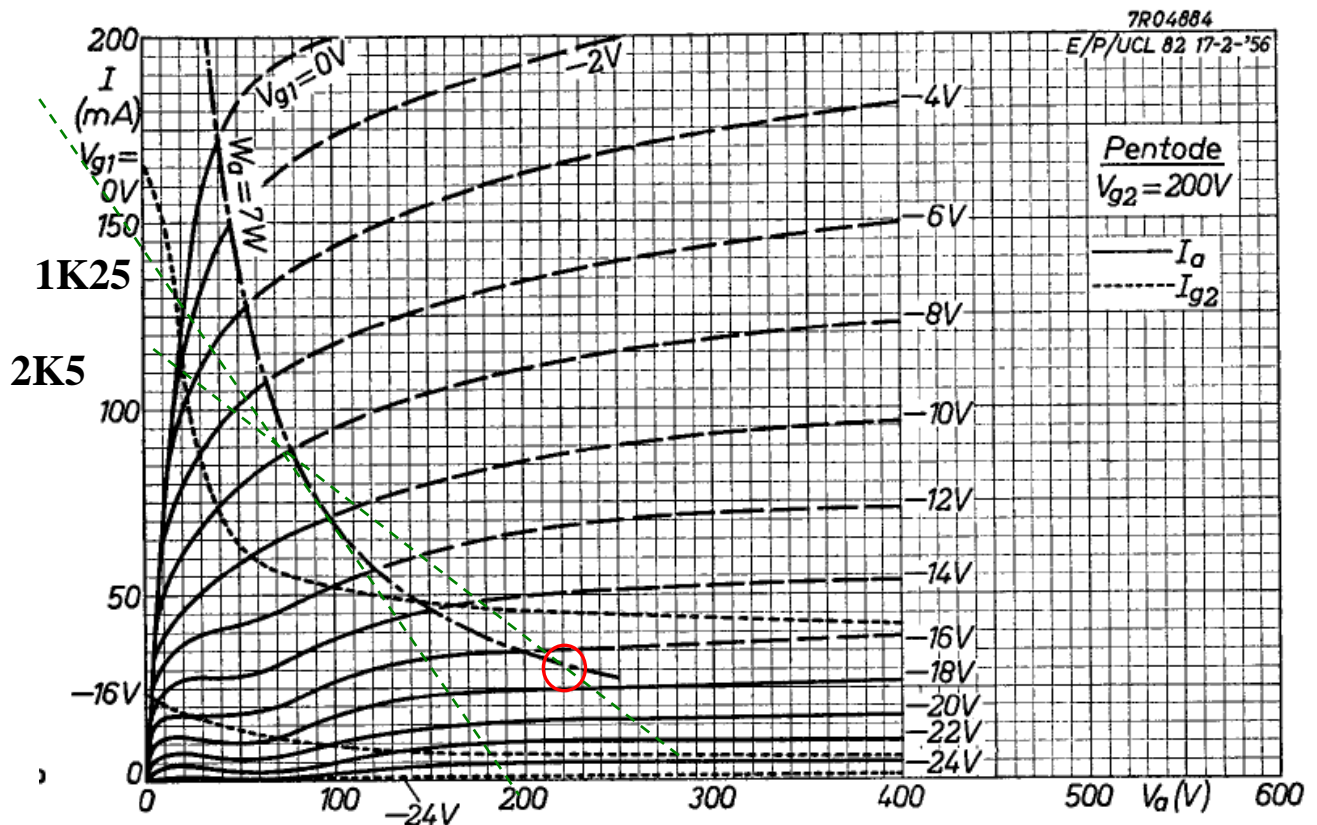
The supply voltage $VS1$ to the output valve plates is about 230V. Plate-cathode voltage will be lower than $VS1$ by an amount up to $\sim 17+3=20V$; ie. OPT half resistance of about 76 Ω and 22 Ω stopper with an idle current of 0.03A, and 17V cathode bias. As the output loading increases, the supply voltage $VS1$ to the output valve plates sags to about 220V. Plate DC voltage will be lower than $VS1$ by an amount up to $\sim 25+11=36V$; ie. OPT half resistance of about 76 Ω and 22 Ω stopper with a peak current of up to about 0.12A, and 25V cathode bias.

Screen voltage supply $VS2$ will vary from about 200V towards 180V under steady-state heavy load. Screen voltage lower than $VS2$ by 17V at idle, and $\sim 25+30=55V$ due to the 1k Ω stopper resistors

at up to 30mA screen current per tube, and the cathode bias voltage. Peak screen power dissipation is then up to $30\text{mA} \times 150\text{V} = 4.5\text{Wpk}$, and about $180 \times 0.008 = 1.4\text{W}$ average.

The maximum output valve bias current allowed is dependent on the maximum recommended plate dissipation of 7W, + 3.2W for the screen, for the 6BM8: $I_{\text{bias(max)}} = P_d / V_b = 7\text{W} / (220-20\text{V}) = 35\text{mA}$.

Assessing the 6BM8 plate curves, which shows the 7W constant power contour, indicates how the amp may dynamically exceed plate max design dissipation levels. Note that these curves are for a 200V screen level, with no compression influences, and the load lines are for 2.5K (5K P-P transformer push-pull) moving to 1.25K.

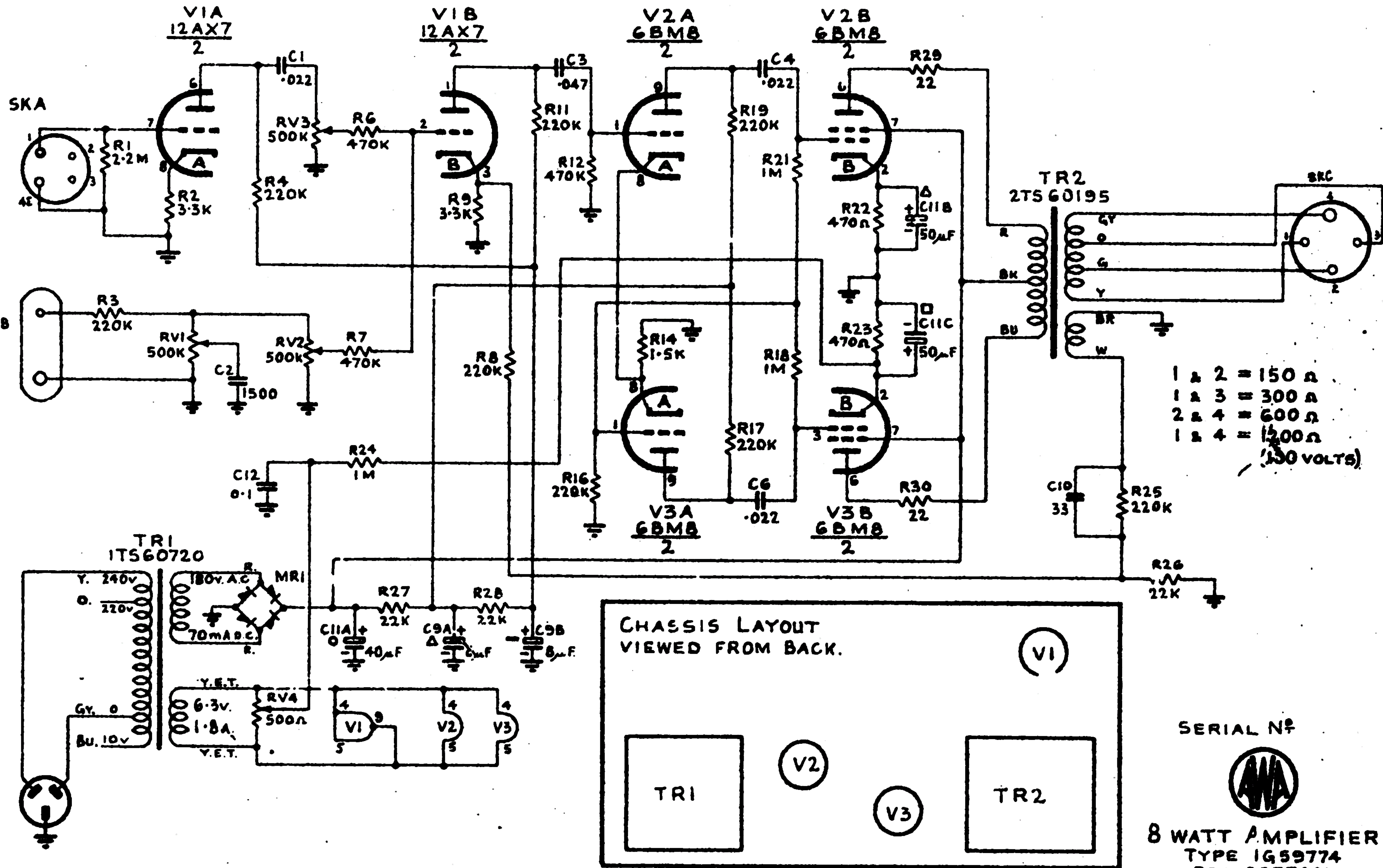


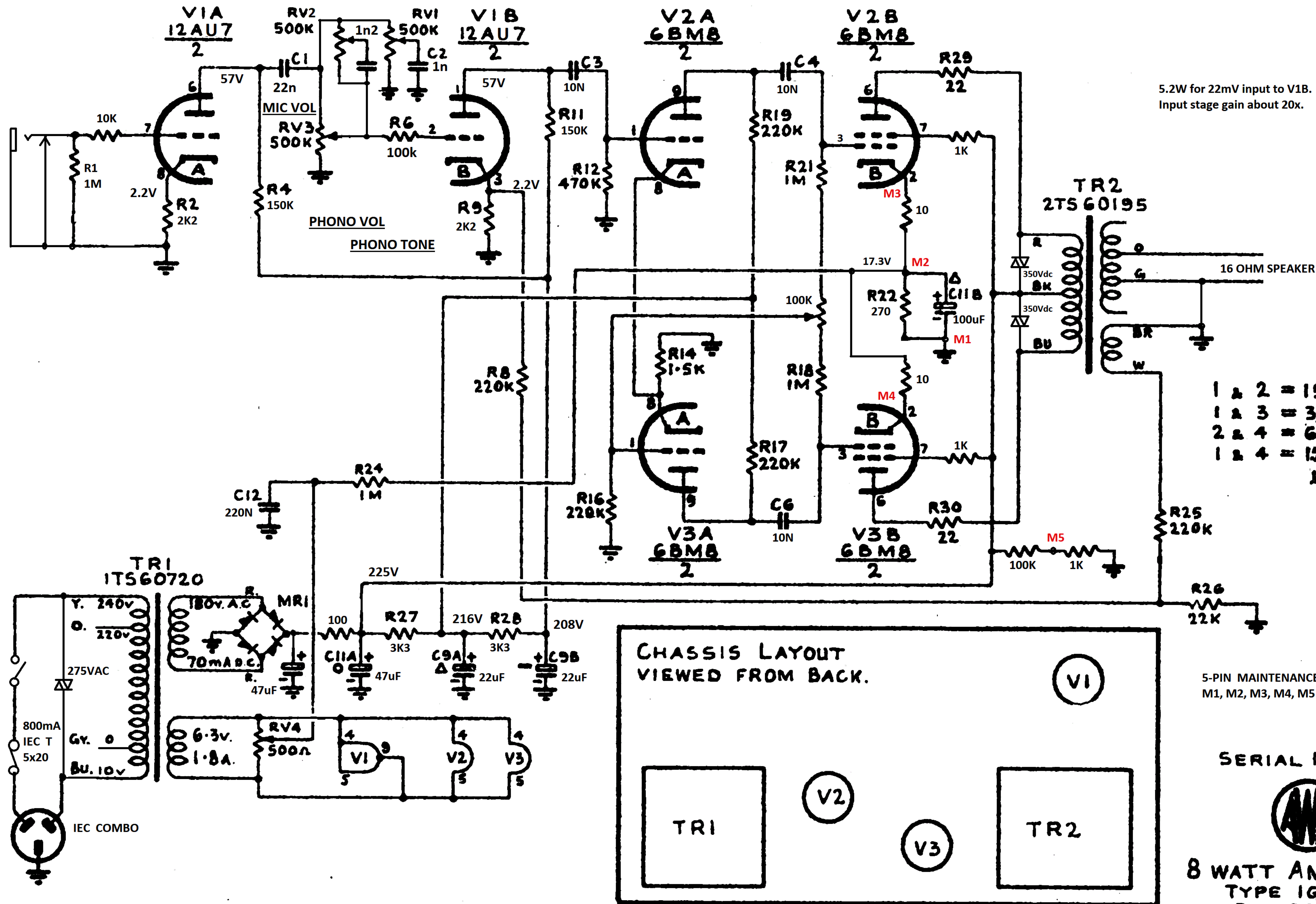
3.3 Power Supplies

The full bridge rectifier circuit uses a 200V secondary HT winding. Only one 6.3VAC secondary is available for heaters. Heater loading is $0.3\text{A} + 2 \times 0.78\text{A} = 1.8\text{A}$.

C11A is replaced with a CRC 47uF, 100Ω, 47uF 450V filter to VS1. A UF4007 full bridge replaced the original bridge.

0V ground is distributed star, with single link to chassis from V1 socket spigot, although another link was used as the speaker output socket could not be easily isolated.







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